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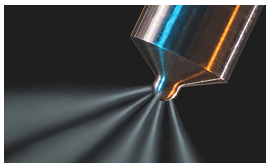
Some new results on the numerical simulation of thick sprays

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Examples : Clouds, Diesel engines, Medical sprays, Nuclear industry, Pharmaceutical industry

Thin sprays:



(a) Diesel engine fuel injector



(b) Medical spray

Thick sprays:

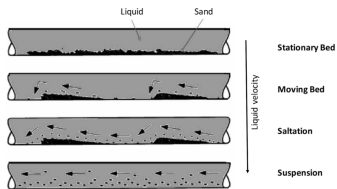
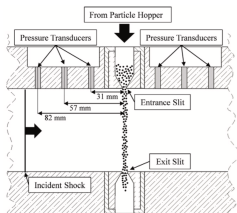


Fig. 1. Sand flow regime in horizontal pipelines.

(c) Leporini et al (2019)



(d) Daniel-Wagner (2022)

- Unknowns for the gas

$$\varrho(t, \mathbf{x}) \geq 0, \quad \mathbf{u}(t, \mathbf{x}) \in \mathbf{R}^3, \quad e(t, \mathbf{x}) \geq 0, \quad \alpha(t, \mathbf{x}) \in (0, 1].$$

- Follow a hyperbolic (compressible Euler equations) or Navier-Stokes equation.
- Unknown for the dispersed phase : kinetic distribution function

$$f(t, \mathbf{x}, \mathbf{v}) \geq 0$$

with \mathbf{v} the velocity of the droplets.

- Follow a Vlasov or Vlasov-Boltzmann (with collision operator) equation

Hypothesis. The particles are monodisperse: all particle have the same radius $r_* > 0$.

Possibility to enrich the model with various effect: internal energy of the droplets, compressibility, rotation of the droplets, inelastic collisions and breakup, chemical reactions...

Euler equations coupled with a Vlasov equation through a friction force

$$\begin{cases} \partial_t \varrho + \nabla_x \cdot (\varrho \mathbf{u}) = 0 \\ \partial_t (\varrho \mathbf{u}) + \nabla_x \cdot (\varrho \mathbf{u} \otimes \mathbf{u}) + \nabla_x p = D_\star \int_{\mathbb{R}^3} (\mathbf{v} - \mathbf{u}) f \, d\mathbf{v} \\ \partial_t f + \mathbf{v} \cdot \nabla_x f + \nabla_v \cdot (\Gamma f) = 0 \\ m_\star \Gamma = -D_\star (\mathbf{v} - \mathbf{u}) \end{cases}$$

with pressure $p = \varrho^\gamma$.

Compressible Vlasov-Euler equation. Coupling through a friction force and volume fraction.

$$\left\{ \begin{array}{l} \partial_t(\alpha \rho) + \nabla_x \cdot (\alpha \rho \mathbf{u}) = 0 \\ \partial_t(\alpha \rho \mathbf{u}) + \nabla_x \cdot (\alpha \rho \mathbf{u} \otimes \mathbf{u}) + \alpha \nabla_x p = D_* \int_{\mathbb{R}^3} (\mathbf{v} - \mathbf{u}) f \, d\mathbf{v} \\ \partial_t(\alpha \rho e) + \nabla_x \cdot (\alpha \rho e \mathbf{u}) + p(\partial_t \alpha + \nabla_x \cdot (\alpha \mathbf{u})) = D_* \int_{\mathbb{R}^3} |\mathbf{v} - \mathbf{u}|^2 f \, d\mathbf{v} \\ \partial_t f + \mathbf{v} \cdot \nabla_x f + \nabla_v \cdot (\Gamma f) = 0 \\ \alpha = 1 - \frac{4}{3} \pi r_*^3 \int_{\mathbb{R}^3} f \, d\mathbf{v} \\ m_* \Gamma = -\frac{4}{3} \pi r_*^3 \nabla_x p - D_* (\mathbf{v} - \mathbf{u}) \end{array} \right.$$

Our interest is in all regime $0 < \alpha \leq 1$.

L. Boudin, L. Desvillettes, and R. Motte. A modeling of compressible droplets in a fluid. Commun. Math. Sci., 1(4):657-669, 2003.

- The mass of each phase is preserved

$$\partial_t(\alpha \rho) + \nabla_x \cdot (\alpha \rho \mathbf{u}) = 0, \quad \partial_t f + \nabla_x \cdot (\mathbf{v} f) + \nabla_v \cdot (\Gamma f) = 0.$$

- The total momentum is preserved

$$\partial_t \left(\alpha \rho \mathbf{u} + \frac{4}{3} \pi r_*^3 \int_{\mathbb{R}^3} f \mathbf{v} \, dv \right) + \nabla_x \cdot \left(\alpha \rho \mathbf{u} \otimes \mathbf{u} + \frac{4}{3} \pi r_*^3 \int_{\mathbb{R}^3} f \mathbf{v} \otimes \mathbf{v} \, dv \right) + \nabla_x p = 0.$$

- The total energy is preserved

$$\begin{aligned} \partial_t \left(\alpha \rho E + \frac{4}{3} \pi r_*^3 \int_{\mathbb{R}^3} f \frac{|\mathbf{v}|^2}{2} \, dv \right) + \nabla_x \cdot \left(\alpha \rho \mathbf{u} E + \frac{4}{3} \pi r_*^3 \int_{\mathbb{R}^3} f \mathbf{v} \frac{|\mathbf{v}|^2}{2} \, dv \right. \\ \left. + \alpha \mathbf{u} p + \frac{4}{3} \pi r_*^3 p \int_{\mathbb{R}^3} f \mathbf{v} \, dv \right) = 0. \end{aligned}$$

- General thermodynamical principles are satisfied since one has

$$\partial_t(\alpha \rho S) + \nabla_x \cdot (\alpha \rho S \mathbf{u}) = \frac{D_*}{T_*} \int_{\mathbb{R}^3} |\mathbf{v} - \mathbf{u}|^2 f \, dv \geq 0.$$

The system rewrites as a system of conservation laws.

- Models
 - in the context of combustion theory introduced in Williams [1985]
 - Classification of sprays O'Rourke [1981]
- Mathematical theory of Thin Sprays ($\alpha \approx 1$):
 - Vlasov-Euler :
 - Local-in-time well posedness for strong solution Baranger and Desvillettes [2006], Mathiaud [2010]
 - Global weak solution in 1D with finite energy Cao [2022]
 - Vlasov-Navier-Stokes :
 - Global existence of weak solution on the 3D-torus Boudin, Desvillettes, Grandmont, and Moussa [2009] and the inhomogenous case Choi and Kwon [2015]
 - Large time behavior studied in Choi [2016], Ertzbischoff, Han-Kwan, and Moussa [2021], Han-Kwan, Moussa, and Moyano [2020]
- Mathematical theory of Thick Sprays ($0 < \alpha \leq 1$) :
 - Boudin, Desvillettes, and Motte [2003].
 - Recent numerical work Benjelloun, Desvillettes, Ghidaglia, and Nielsen [2012]
 - Linear stability studied in Buet, Després, and Desvillettes [2023]
 - Local Well-posedness for regularized model Buet, Després, and F [2022]
 - Very recently, Local in time Well-posedness for the Navier Stokes (with diffusion) case and Penrose stable initial data Ertzbischoff and Han-Kwan [2023]

$$\left\{ \begin{array}{l} \partial_t(\alpha \varrho) + \nabla_x \cdot (\alpha \varrho \mathbf{u}) = 0 \\ \partial_t(\alpha \varrho \mathbf{u}) + \nabla_x \cdot (\alpha \varrho \mathbf{u} \otimes \mathbf{u}) + \alpha \nabla_x p = D_* \int_{\mathbb{R}^3} (\mathbf{v} - \mathbf{u}) f \, d\mathbf{v} \\ \partial_t(\alpha \varrho e) + \nabla_x \cdot (\alpha \varrho e \mathbf{u}) + p(\partial_t \alpha + \nabla_x \cdot (\alpha \mathbf{u})) = D_* \int_{\mathbb{R}^3} |\mathbf{v} - \mathbf{u}|^2 f \, d\mathbf{v} \\ \partial_t f + \mathbf{v} \cdot \nabla_x f + \nabla_v \cdot (\Gamma f) = 0 \\ \alpha = 1 - \frac{4}{3} \pi r_*^3 \int_{\mathbb{R}^3} f \, d\mathbf{v} \\ m_* \Gamma = -\frac{4}{3} \pi r_*^3 \nabla_x p - D_*(\mathbf{v} - \mathbf{u}) \end{array} \right.$$

■ Theory

- No Cauchy theory available: Loss of regularity in the equations

$$\partial_t(\alpha \varrho) + \nabla_x \cdot (\alpha \varrho \mathbf{u}) = 0 \Rightarrow \|\varrho\|_{H^k} \lesssim \|f\|_{H^{k+1}},$$

$$\partial_t f + \mathbf{v} \cdot \nabla_x f + \nabla_v \cdot (\Gamma f) = 0 \Rightarrow \|f\|_{H^k} \lesssim \|\varrho\|_{H^{k+1}},$$

$$\Rightarrow \|\varrho\|_{H^k} \lesssim \|\varrho\|_{H^{k+2}}, \quad \|f\|_{H^k} \lesssim \|f\|_{H^{k+2}}.$$

Two way to overcome loss of regularity: system with diffusion $\nu \Delta u$, system with regularization: $\nabla_x p \rightarrow \langle \nabla_x p \rangle$.

- No usual definition of weak solution in L^P :

$$\nabla_v \cdot (\Gamma f) = -\nabla_x p(\varrho, e) \cdot \nabla_v f - \nabla_v \cdot ((\mathbf{v} - \mathbf{u})f)$$

■ Numerics

- Problem of the positivity of the volume fraction

We work on the barotropic system in 1D with periodic boundary conditions:

$$(1) \quad \begin{cases} \partial_t(\alpha \varrho) + \partial_x(\alpha \varrho u) = 0 \\ \partial_t(\alpha \varrho u) + \partial_x(\alpha \varrho u^2) + \alpha \partial_x p = \int_{\mathbf{R}} (v - u) f \, dv \\ \partial_t f + v \partial_x f + \partial_v(\Gamma f) = 0 \\ \alpha = 1 - \int_{\mathbf{R}} f \, dv \\ \Gamma = -\partial_x p - (v - u) \\ p(\varrho) = \varrho^\gamma, \gamma > 1. \end{cases}$$

The system (1) can be rewritten as a system of conservation laws

$$(2) \quad \begin{cases} \partial_t(\alpha \varrho) + \partial_x(\alpha \varrho u) = 0 \\ \partial_t \left(\alpha \varrho u + \int_{\mathbf{R}} f v \, dv \right) + \partial_x \left(\alpha \varrho u^2 + p(\varrho) + \int_{\mathbf{R}} v^2 f \, dv \right) = 0 \\ \partial_t f + v \partial_x f + \partial_v((- \partial_x p + u) f - v f) = 0 \\ p(\varrho) = \varrho^\gamma, \gamma > 1. \end{cases}$$

The fluid part of the system will be written as $\partial_t \mathbf{U} + \partial_x \mathbf{F}(\mathbf{U}, f) = 0$ with

$$\mathbf{U} = \begin{pmatrix} \alpha \varrho \\ \alpha \varrho u + \int_{\mathbf{R}} f v \, dv \end{pmatrix} \text{ and } \mathbf{F}(\mathbf{U}, f) = \begin{pmatrix} \alpha \varrho u \\ \alpha \varrho u^2 + p + \int_{\mathbf{R}} f v^2 \, dv \end{pmatrix}.$$

Objective: Write a conservative scheme that preserves the positivity of the volume fraction $\alpha(t, x) > 0$.

- The conservative form of the fluid part allow us to use classical hyperbolic scheme (e.g: Rusanov, HLL...).
- For the Vlasov equation, a possible choice is semi-Lagrangian method based on polynomial interpolation.

We use here the splitting scheme:

- 1 Solve $\partial_t \mathbf{U} + \partial_x \mathbf{F}(\mathbf{U}, f) = 0$
- 2 Solve $\partial_t f + v \partial_x f = 0$
- 3 Solve $\partial_t f + (u - \partial_x p) \partial_v f = 0$
- 4 Solve $\partial_t f - \partial_v (vf) = 0$

CFL condition. Compute the eigenvalues of the fluid part:

$$\lambda_{\pm} = u \pm \sqrt{\frac{p'(\varrho)}{\alpha}}, \quad \max(\lambda_{\pm}) \frac{\Delta t}{\Delta x} \leq \frac{1}{2}.$$

Recall the formula of the volume fraction

$$\alpha(t, x) = 1 - \int_{\mathbf{R}} f(t, x, v) dv > 0$$

Problem: Solve the free transport equation with constraint

$$\begin{cases} \partial_t f(t, x, v) + v \partial_x f(t, x, v) = 0 \\ 0 \leq \int_{\mathbf{R}} f(t, x, v) dv < 1 \\ \iint_{\mathbf{T} \times \mathbf{R}} f(t, x, v) dx dv = \iint_{\mathbf{T} \times \mathbf{R}} f_0(x, v) dx dv \end{cases}$$

Strategy: Prediction-Correction scheme

- After a Prediction step $\tilde{f}^{n+1}(x, v) = f^n(x - \Delta t v, v)$, do **Correction** step: project on a set of admissible density $f^{n+1}(x, v) = P(\tilde{f}^{n+1}(x, v))$ in a **conservative** way
- The projection is made following ideas from the modelisation of crowd motion

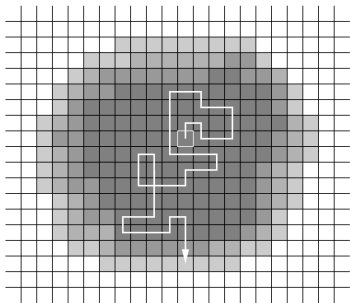


Figure: Random walk transporting the exceeding mass (Maury et al).

In a cell where the constraint is violated, do

- 1 Start a random walk from the cell transporting the exceeding mass
- 2 When the random walk encounters a cell where the density is admissible, get rid of as much mass as it can
- 3 Continue until the exceeding mass is zero

Bertrand Maury, Aude Roudneff-Chupin, Filippo Santambrogio, Juliette Venel. Handling congestion in crowd motion modeling. *Networks and Heterogeneous Media*, 2011, 6(3): 485-519. doi: 10.3934/nhm.2011.6.485

The Thick Sprays system **without** friction

$$\begin{cases} \partial_t(\alpha\rho) + \nabla_x \cdot (\alpha\rho\mathbf{u}) = 0 \\ \partial_t(\alpha\rho\mathbf{u}) + \nabla_x \cdot (\alpha\rho\mathbf{u} \otimes \mathbf{u}) + \alpha\nabla_x p = 0 \\ \partial_t f + \mathbf{v} \cdot \nabla_x f - \nabla_x p(\rho) \cdot \nabla_v f = 0 \end{cases}$$

has similarity with the Vlasov-Poisson system

$$\begin{cases} \partial_t f + \mathbf{v} \cdot \nabla_x f - \mathbf{E} \cdot \nabla_v f = 0, \\ -\Delta\varphi = \int_{\mathbf{R}^3} f \, dv - 1 \\ \mathbf{E}(t, \mathbf{x}) = -\nabla_x \varphi(t, \mathbf{x}) \end{cases}$$

- What strongly differs is the **regularity** of the pressure vs the regularity of the electric potential.
- Some techniques used for linearized Vlasov-Poisson transfer to Thick Sprays equations.

$$f_0(x, v) = (1 + \varepsilon \cos(kx))e^{-v^2/2}$$

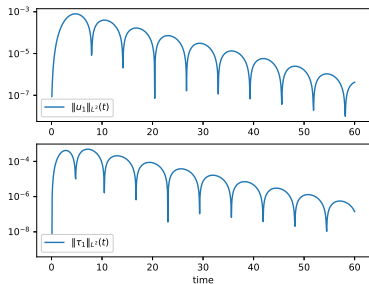


Figure: Decay of acoustic energy for Thick Sprays

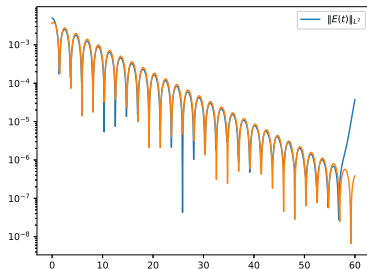


Figure: Decay of electric field for Vlasov-Poisson

Linearize the system **without friction** $D_* = 0$ around $\varrho_0(x) = cte$, $u_0(x) = 0$, $f^0(v) = e^{-v^2/2}$

$$\begin{cases} \varrho(t, x) = \varrho_0 & +\varepsilon\varrho_1(t, x) & +O(\varepsilon^2) \\ u(t, x) = & \varepsilon u_1(t, x) & +O(\varepsilon^2) \\ \alpha(t, x) = \alpha_0 & +\varepsilon\alpha_1(t, x) & +O(\varepsilon^2) \\ f(t, x, v) = f^0 & +\varepsilon f_1(t, x, v) & +O(\varepsilon^2) \end{cases}$$

Regrouping the linearized equations for $\tau_1 = \frac{-\varrho_1}{\varrho_0}$, u_1 and f_1 , one gets, setting the constants to one

$$\begin{cases} \partial_t \tau_1 = \partial_x u_1 + \partial_x \int_{\mathbf{R}} v f_1 \, dv \\ \partial_t u_1 = \partial_x \tau_1 \\ \partial_t f_1 + v \partial_x f_1 - \partial_v f^0 \partial_x \tau_1 = 0 \end{cases}$$

For Landau damping in Vlasov-Poisson, it is well known that for a given k , the rate of decay are given by the root in the complex plane of the dispersion function

$$\mathcal{D}_{VP}(\omega, k) = 1 - \frac{1}{k^2} \int_{-\infty}^{+\infty} \frac{\partial_v f^0(v)}{v - \frac{\omega}{k}} dv$$

Similar formal computation gives us a dispersion function for Thick Sprays

$$\mathcal{D}_{TS}(\omega, k) = 1 - \frac{k^2}{\omega^2} + \frac{k}{\omega} \int_{-\infty}^{+\infty} \frac{v \partial_v f^0(v)}{v - \frac{\omega}{k}} dv$$

Initial condition:

$$\varrho(t=0, x) = 1, \quad u(t=0, x) = 0, \quad f(t=0, x, v) = \frac{1}{\sqrt{2\pi}}(1 + \varepsilon \cos(kx))e^{-v^2/2}$$

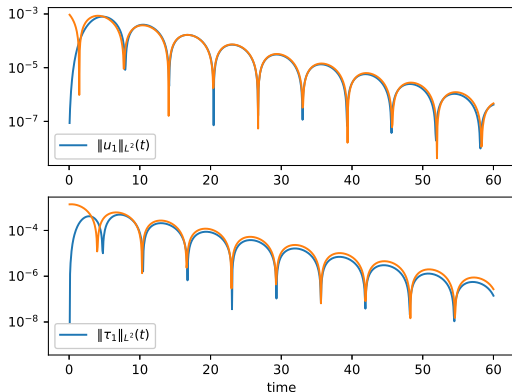


Figure: Decay of the acoustic energy, $\Im(\omega) = -0.13$, $\Re(\omega) = 0.497$

- Presentation of a conservative method to preserve maximum principle for the volume fraction.
- Landau damping phenomenon in the frictionless system.
- Investigate the role of the friction.

Adapt this method in the kinetic case: The constraint is not of the type $a \leq f(t, x) \leq b$ but $a \leq \int_{\mathbf{R}} f(t, x, v) dv \leq b$. After the Prediction step $\tilde{f}^{n+1}(x, v) = f^n(x - \Delta tv, v)$, do

- 1 Start from a cell x_i where $\tilde{\alpha}_i^{n+1} < \alpha_{\min}$
- 2 Compute the exceeding mass Δm_i^0 . Modify the value, $\forall j$,

$$f_{i,j}^{n+1} = \frac{1 - \alpha_{\min}}{\frac{4}{3}\pi r_*^3} \frac{\tilde{f}_{i,j}^{n+1}}{\sum_k \Delta v_k \tilde{f}_{i,k}^{n+1}}$$

, so that $\alpha_i^{n+1} = \alpha_{\min}$

- 3 Start a random walk (S_m), when the walk meet a cell S_m such that $\tilde{\alpha}_{S_m}^{n+1} > \alpha_{\min}$, get rid of as much mass as possible and modify

$$f_{S_m,j}^{n+1} = \min \left(\sum_k \Delta v_k \tilde{f}_{S_m,j}^{n+1} + \Delta m_i^0, \frac{1 - \alpha_{\min}}{\frac{4}{3}\pi r_*^3} \right) \frac{\tilde{f}_{S_m,j}^{n+1}}{\sum_k \Delta v_k \tilde{f}_{S_m,k}^{n+1}}$$

When all the exceeding mass has been distributed, the volume fraction α_i^{n+1} is admissible.

- Necessity to add a small minimum value α_{\min} (e.g 10^{-3} ...) because $\alpha = 0$ is not an admissible value, can correspond to a close-packing limit.

Note that no convergence result of this algorithm is known

By construction, this method is conservative

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